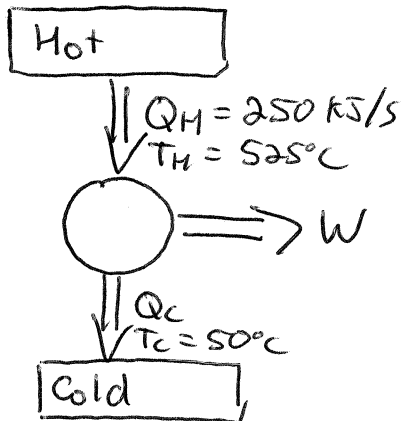


5.2



Definition of efficiency

$$\eta = 1 - \frac{T_c}{T_H} = 1 - \frac{50+273}{525+273} = 0.59$$

$$\eta = \frac{W}{Q_H}$$

$$W = \eta Q_H = 0.59 \times 250 = 148.8 \text{ kJ/s}$$

From 1st law energy balance

$$Q_c = Q_H - W = 250 - 148.8 = 101.2 \text{ kJ/s}$$

5.3

$$W = 95000 \text{ kW}$$

$$a) \eta = 1 - \frac{300}{750} = 0.6$$

$$Q_H = \frac{W}{\eta} = \frac{95000}{0.6} = 1.58 \times 10^5 \text{ kW}$$

$$Q_c = Q_H - W = 6.3 \times 10^4 \text{ kW}$$

$$b) Q_H = \frac{W}{\eta} = \frac{95000}{0.35} = 2.7 \times 10^5 \text{ kW}$$

$$Q_c = 1.76 \times 10^5 \text{ kW}$$

5.4

$$\eta_{\text{carnot}} = 1 - \frac{30 + 273}{350 + 273} = 0.51$$

a)  $\eta_{\text{actual}} = 0.55 \times 0.51 = 0.28$

b)  $\eta_{\text{actual}} = 0.55 \times \left(1 - \frac{30 + 273}{T}\right) = 0.35$

$$T = 833 \text{ K} = 560^\circ\text{C}$$

5.6

$$\eta = 1 - \frac{T_c}{T_H}$$

$$\left(\frac{\partial \eta}{\partial T_c}\right)_{T_H} = \frac{-1}{T_H} \quad \text{and} \quad \left(\frac{\partial \eta}{\partial T_H}\right)_{T_c} = \frac{T_c}{T_H^2} = \frac{T_c}{T_H} \times \frac{1}{T_H}$$

Since  $\frac{T_c}{T_H}$  is less than 1,  $\eta$  changes faster with  $T_c$  than

with  $T_H$   $\therefore$  in theory more effective to change  $T_c$  and  $T_H$

In practice,  $T_c$  is fixed by the environment and it is more practical to change  $T_H$

5.9

$$n = \frac{P_1 V}{R T_1} = 1.443 \text{ mol}$$

$$Q = 15000 \text{ J}$$
$$C_v = \frac{5}{2} \times R$$

a) constant volume heating

$$\Delta u = Q + w^0 = Q = n C_v (T_2 - T_1)$$

$$T_2 = T_1 + \frac{Q}{n C_v} = 500 + \frac{15000}{1.443 \times \left(\frac{5}{2} \times 8.314\right)} = 1 \times 10^3 \text{ K}$$

$$\Delta S = n \left( C_p \ln \frac{T_2}{T_1} - R \ln \frac{P_2}{P_1} \right)$$

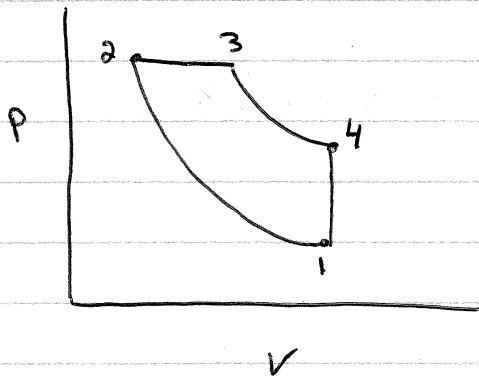
$$\text{But } \frac{P_2}{P_1} = \frac{T_2}{T_1}$$

$$\Delta S = n \left[ (C_p - R) \ln \left( \frac{T_2}{T_1} \right) \right] = n C_v \ln \frac{T_2}{T_1} = 1.443 \times \frac{5}{2} \times 8.314 \times \ln \left( \frac{1000}{500} \right)$$

$$\boxed{\Delta S = 20.794 \text{ J/K}}$$

b) Entropy change of the gas is the same since  $T_2$  is the same

5.19



For adiabatic steps  $1 \rightarrow 2$  and  $3 \rightarrow 4$

$$T_1 V_1^{\gamma-1} = T_2 V_2^{\gamma-1} \quad T_3 V_3^{\gamma-1} = T_4 V_4^{\gamma-1}$$

where  $\gamma = C_p/C_v$

For isochoric step  $4 \rightarrow 1$

$$V_4 = V_1$$

For isobaric step  $2 \rightarrow 3$

$$\frac{T_2}{V_2} = \frac{T_3}{V_3}$$

$$\text{Thermal efficiency} = \eta = \frac{Q_H + Q_C}{Q_H} = 1 + \frac{Q_C}{Q_H}$$

For step  $2 \rightarrow 3$

$$Q_{23} = C_p(T_3 - T_2) = Q_H$$

For step  $4 \rightarrow 1$

$$Q_{41} = C_v(T_1 - T_4) = Q_C$$

~~$T_1 = T_2 = V_3$~~

$$\eta = 1 + \frac{C_v (T_1 - T_4)}{C_p (T_3 - T_2)} = 1 + \frac{1}{\gamma} \frac{(T_1 - T_4)}{(T_3 - T_2)}$$

$$T_1 = 200^\circ\text{C} \quad T_2 = 1000^\circ\text{C} \quad T_3 = 1700^\circ\text{C} \quad T_4 = ?$$

$\therefore$  we need  $T_4$

$$T_4 = T_3 \frac{V_3^{\gamma-1}}{V_4^{\gamma-1}}$$

$$\frac{T_1}{T_2} = \frac{V_2^{\gamma-1}}{V_1^{\gamma-1}} = \frac{V_2^{\gamma-1}}{V_4^{\gamma-1}}$$

$$V_2 = \frac{T_2}{T_3} V_3$$

$$\frac{T_1}{T_2} = \left(\frac{T_2}{T_3}\right)^{\gamma-1} \frac{V_3^{\gamma-1}}{V_4^{\gamma-1}}$$

$$\frac{T_1 T_3^{\gamma-1}}{T_2 T_2^{\gamma-1}} = \frac{V_3^{\gamma-1}}{V_4^{\gamma-1}}$$

$$T_4 = \frac{T_3 T_1}{T_2} \frac{T_3^{\gamma-1}}{T_2^{\gamma-1}} = \frac{1973 \times 473}{1273} \times \frac{1973^{0.4}}{1273^{0.4}} = 873.5 \text{ K}$$

$$\therefore \eta = 1 + \frac{1}{1.4} \frac{(473 - 873)}{(1973 - 1273)} = 0.59$$

FYI: This cycle is the same cycle a standard Diesel engine uses.

S.26

$$T = 403.15 \text{ K} \quad P_1 = 2 \text{ bar} \quad P_2 = 6.5 \text{ bar} \quad T_{\text{res}} = 298.15 \text{ K}$$

$$\Delta S_{\text{gas}} = -R \ln \left( \frac{P_2}{P_1} \right) = -7.944 \frac{\text{J}}{\text{mol K}}$$

→ isothermal  
compression

$$\text{Irreversible work} = W_{\text{irr}} = 1.3 \times W_{\text{rev}} = 1.3 \times RT \ln \left( \frac{P_2}{P_1} \right)$$

$$W_{\text{irr}} = 4.163 \times 10^3 \text{ J/mol}$$

$$\Delta U = W + Q \quad Q = -W \quad (\text{note: } Q \text{ here is with respect to system})$$

$$\Delta S_{\text{res}} = \frac{-Q}{T_{\text{res}}} = \frac{4.163 \times 10^3}{298.15} = 13.96 \frac{\text{J}}{\text{mol K}}$$

$$\Delta S_{\text{total}} = \Delta S_{\text{gas}} + \Delta S_{\text{res}} = 6.02 \frac{\text{J}}{\text{mol K}}$$

5.27: Data from NIST chemistry web book (all values in J/K)

> **restart;**

For SO2:

> **A\_so2:=21.43049;B\_so2:=74.35094;C\_so2:=-57.75217;D\_so2:=16.35534;E\_so2:=0.086731;**

*A\_so2* := 21.43049

*B\_so2* := 74.35094

*C\_so2* := -57.75217

*D\_so2* := 16.35534

*E\_so2* := 0.086731

> **dS\_so2:=10\*int((A\_so2 + B\_so2\*(T/1000) + C\_so2\*(T/1000)^2 + D\_so2\*(T/1000)^3 + E\_so2/((T/1000)^2))/T,T=473..1373);**

*dS\_so2* := 554.8333486

For propane: (Shomate equation not available but Cp vs T data is available so using excel to fit polynomial to this data and integrating):

> **Cp\_propane:=-7e-5\*T^2+0.2372\*T+10.535;**

*Cp\_propane* := -0.00007  $T^2$  + 0.2372  $T$  + 10.535

> **dS\_propane:=12\*int(Cp\_propane/T,T=250+273..1200+273);**

*dS\_propane* := 2038.580743

>

5.28: Data from NIST chemistry web book (all values in J/K)

Step 1: Find final temperature:  $H(200C)-H(T) = Q$

> **restart;**

a) To find T2, must iterate until  $dH = 800kJ$

> **A\_ethylene:=-6.387880;B\_ethylene:=184.4019;C\_ethylene:=-112.9718;D\_ethylene:=28.49593;E\_ethylene:=0.315540;**

*A\_ethylene* := -6.387880

*B\_ethylene* := 184.4019

*C\_ethylene* := -112.9718

*D\_ethylene* := 28.49593

*E\_ethylene* := 0.315540

> **dH\_ethylene:=10\*int(A\_ethylene + B\_ethylene\*(T/1000) + C\_ethylene\*(T/1000)^2 + D\_ethylene\*(T/1000)^3 +E\_ethylene/((T/1000)^2),T=473..1379);**

*dH\_ethylene* := 7.999539313 10<sup>5</sup>

So, T2=1379K. dS is in J/K

> **dS\_ethylene:=10\*int((A\_ethylene + B\_ethylene\*(T/1000) + C\_ethylene\*(T/1000)^2 + D\_ethylene\*(T/1000)^3 +E\_ethylene/((T/1000)^2))/T,T=473..1379);**

*dS\_ethylene* := 899.8052812

b) To find T2, follow the same instructions as in part a) except  $dH=2500$

> **Cp\_1butene:=2e-8\*T^3-0.0001\*T^2+0.2823\*T+12.979;**

*Cp\_1butene* := 2 10<sup>-8</sup> T<sup>3</sup> - 0.0001 T<sup>2</sup> + 0.2823 T + 12.979

> **dH\_1butene:=15\*int(Cp\_1butene,T=260+273..1350);**

*dH\_1butene* := 2.504840530 10<sup>6</sup>

So T2=1350K. dS is in J/K

> **dS\_1butene:=15\*int(Cp\_1butene/T,T=260+273..1350);**

*dS\_1butene* := 2717.602062

c) To find T2, follow same instructions as in part a) and b) but this time  $dH=1E6$  KJ. T1=260C, n=18143.68mol

> **dH\_ethylene\_c:=18143\*int(A\_ethylene + B\_ethylene\*(T/1000) + C\_ethylene\*(T/1000)^2 + D\_ethylene\*(T/1000)^3 +E\_ethylene/((T/1000)^2),T=260+273..1180);**

*dH\_ethylene\_c* := 1.005952861 10<sup>9</sup>

So T2=1180K. dS is in J/K

> **dS\_ethylene:=18143\*int((A\_ethylene + B\_ethylene\*(T/1000) + C\_ethylene\*(T/1000)^2 + D\_ethylene\*(T/1000)^3 +E\_ethylene/((T/1000)^2))/T,T=260+273..1180);**

